

% Bering Strait 2014 NORSEMAN2 log CTD

%example from 2013

%Date	Time	1	Cast NO	Down	Depth (m)	Lat (deg)	Lat (min)	Lon (deg)	Lon(min)	%	StationID	Windspeed	Winddir	Operator	Comments
20130704	0627	1	1	1	52.5	65	21.690	167	53.450	%	testcast	14.4	182	ACPF	Test cast en route to BS line
20130704	0635	1	1	2	52.5	65	21.000	167	53.650	%		5.7	51	ACPF	1, 5 ans 6 are leaking
20130704	0713	1	2	1	42.2	65	25.100	167	59.270	%	testcast2	15.6	197	ACPF	This is to test bottles - All bottles OK
20130704	0721	1	2	2	42.2	65	25.175	167	59.260	%				ACPF	

%Date Time 1 Cast NO Down Depth (m) Lat (deg) Lat (min) Lon (deg) Lon(min) % StationID Windspeed Winddir Operator Comments

%Please fill in all data for every event (CTD/net tow) %

%There should be one line for the beginning of the event and one line for the end %

%Date is GMT and has the format yyyyymmdd %

%Time is GMT and has the format hhmm %

%Ty=Type: 1=CTD / 2=Net tow/4=prod cast x %

THIS YEAR WE ONLY HAVE TYPE 1 %

%#,Number is consecutive for that event type %

%In/out (I/O): 1=In / 2=Out %

%Dep=waterdepth(m) from Furuno readout by CTD which is depth below keel, keel is 3m (10ft) %

%LatD and LatM are Latitude Degrees and Minute and are positive N %

%LonD and LonM are Longitude Degrees and Min and are positive W %

%St is the name of the station (Line ID then station number) %

%SS = CTD operator estimate of sea state (Beaufort Scale)

%WSp=wind speed in m/s; WD=Wind direction from bridge

%Op=CTD operator

% when 3 lines for NET, dep indicates wire out for net

%Fill in any comments if needed. %

%Date	Time	1	Cast NO	Down	Depth (m)	Lat (deg)	Lat (min)	Lon (deg)	Lon(min)	%	StationID	Knots Windspeed	deg (0=N) Winddir	Operator	Comments
20140630	2035	1	1	1	17.3	64	43.774	166	41.009	%	dry test	3.4	217	atn	dry test to learn CTD driving
20140630	2045	1	1	2	17.1	64	44.855	166	43.033	%	dry test	4.6	214	atn	surface only as pump didn't work
% put in water, but pump didn't come on. Tried several things, brought it on board, overwrote those test, finally got pump turned on manually in air (saved as cast 2)															
20140630	2151	1	2	1		64		166		%	dry test			RJD	final dry test with pump on manually in air
20140630	2155	1	2	2		64		166		%	dry test			RJD	
20140630	2250	1	3	1		64		166		%	wet test			RJD	try again in water automatically, pump not on
20140630	2251	1	3	2		64		166		%	wet test			RJD	
20140630	2252	1	4	1		64	57.255	167		%	wet test	calm		RJD	still in water, turned on pumps manually, went to depth
20140630	2259	1	4	2	10.7	64	57.36	167	4.63	%	wet test			RJD	altimeter ok

% Noticed previous casts were with old cal, updated cals to 2012

20140701	43	1	5	1	17.4	65		167		%	wet test			ACPF	try again for automatic pump, but didn't work
20140701	46	1	5	2		65		167		%	wet test			ACPF	
20140701	48	1	6	1	17.2	65	8.05	167	25.67	%	wet test			ACPF	still in water, redo manually, ok
20140701	54	1	6	2		65		167		%	wet test			ACPF	BUT altimeter does not change with depth

% altimeter stuck at 18m (close to range from surface), but didn't change with depth - so moved altimeter down

20140701	102	1	7	1	17.1	65	8	167	25	%	wet test			ACPF	testing lowered altimeter - still bad
20140701	103	1	7	2		65		167		%	wet test			ACPF	

% decide can live with turning pump on manually, as obvious things don't make automatic work - **** TEST THIS BACK IN SEATTLE****

% trying to fix altimeter - added extra 20lbs weight (in case wasn't straight in water), replugged cables

20140701	1542	1	8	1	44.5	65	44.63	168	15.16	%	Calcast recovery site A4_13			ACPF	To 45 m. Altimeter reading 99m, winch wo ok to within 2m
20140701	1545	1	8	2		65	44.87	168	15.14	%					
20140701	1658	1	9	1	52.9	65	46.72	168	33.9	%	Cal cast recovery site A2			ACPF	To 54 m. Altimeter ok at surface, then stuck.
20140701	1701	1	9	2		65	46.88	168	33.9	%					(Altimeter connectors cleaned pre cast)

% Here we added the turbidity measurements (Calib as of March 11, 2010) to the table plot (upper right). There is no graph of turbidity.

% We have updated xmlcom file and psa files to Version 3 (BStrait2014vers30thJune2014_v3.psa and *_v3.xmlcom)

20140702	102	1	10	1	54.3	66	19.709	168	57.13	%	Cal cast recovery site A3	20.9	186	RJD	
20140702	108	1	10	2	54.4	66	19.919	168	57.22	%		14.2	169.5	RJD	
20140702	1930	1	11	1	54.4	66	19.635	168	56.855	%	Cal cast deployment A3	15.7	202	ACPF	
20140702	1935	1	11	2	54.4	66	19.767	168	56.892	%		14.4	193	atn	
20140703	105	1	12	1	53.2	65	46.805	168	33.782	%	Cal cast deployment A2	14.8	192	RJD	
20140703	109	1	12	2	54.2	65	46.957	168	33.678	%	Cal cast deployment A2	14.9	192	RJD	

20140703	234	1	13	1	44.9	65	44.72	168	15.207 %	Cal cast deployment A4	18.4	206	RJD	
20140703	237	1	13	2	45	65	44.83	168	15.157 %	Cal cast deployment A4	18.8	196	RJD	
20140703	451	1	14	1	27.9	65	35.025	168	7.447 %	BS24	10.9	168	atn	very fast current
20140703	454	1	14	2	28.5	65	35.122	168	7.685 %	BS24	16.6	152	atn	
20140703	504	1	15	1	30.3	65	36.092	168	9.96 %	BS23	17.4	172	atn	
20140703	506	1	15	2	30.7	65	36.203	168	10.278 %	BS23	18.3	164	atn	
20140703	518	1	16	1	29.5	65	37.484	168	10.622 %	BS22	19	185	atn	
20140703	518	1	16	2	29.8	65	37.589	168	10.689 %	BS22	19.8	189	atn	
20140703	539	1	17	1	40.2	65	38.594	168	14.94 %	BS21	19.8	176	atn	
20140703	541	1	17	2	40.4	65	38.681	168	14.977 %	BS21	19.1	177	atn	
20140703	557	1	18	1	46.4	65	39.271	168	19.001 %	BS20	15.8	190	atn	
20140703	600	1	18	2	46.6	65	39.359	168	19.008 %	BS20	18.4	183	atn	
20140703	618	1	19	1	49.8	65	40.323	168	23.518 %	BS19	17.7	193	atn	
20140703	620	1	19	2	49.9	65	40.412	168	23.551 %	BS19	17.8	190	atn	
20140703	642	1	20	1	51.8	65	41.144	168	26.929 %	BS18	16.6	187	atn	
20140703	645	1	20	2	52.5	65	41.235	168	26.937 %	BS18	16.8	184	atn	BStrait14020.hdr error: station should be BS18, not BS20
20140703	658	1	21	1	52.1	65	41.687	168	29.004 %	BS17S	16.1	185	atn	
20140703	701	1	21	2	51.6	65	41.782	168	28.978 %	BS17S	16.5	188	atn	
20140703	713	1	22	1	52.9	65	42.183	168	31.347 %	BS17	15.4	187	atn	
20140703	716	1	22	2	53	65	42.238	168	31.39 %	BS17	15.4	187	atn	
20140703	737	1	23	1	49.9	65	43.269	168	35.537 %	BS16	15.5	196	atn	
20140703	739	1	23	2	50	65	43.352	168	35.56 %	BS16	16.2	190	atn	
20140703	803	1	24	1	50.2	65	44.367	168	40.032 %	BS15	14.1	187	atn	
20140703	806	1	24	2	50.2	65	44.433	168	39.932 %	BS15	15	193	atn	
20140703	824	1	25	1	51.1	65	45.273	168	43.331 %	BS14	16.4	193	atn	
20140703	826	1	25	2	51.1	65	45.329	168	43.379 %	BS14	17.3	188	atn	
20140703	847	1	26	1	50.1	65	46.351	168	47.607 %	BS13	17.3	186	atn	
20140703	849	1	26	2	50.1	65	46.432	168	47.672 %	BS13	17.1	184	atn	
20140703	910	1	27	1	42.9	65	47.245	168	51.597 %	BS12	24	181	atn	
20140703	913	1	27	2	42.8	65	47.313	168	51.643 %	BS12	24.8	178	atn	
20140703	932	1	28	1	45.6	65	48.316	168	55.867 %	BS11	20.7	192	atn	T/S vertically constant!
20140703	934	1	28	2	45.7	65	48.396	168	55.879 %	BS11	24.1	190	atn	
20140703	944	1	29	1	45.8	65	49.279	168	56.099 %	DL1	19.6	188	atn	T/S still near constant vertically
20140703	946	1	29	2	45.9	65	49.366	168	56.021 %	DL1	20.8	188	atn	
20140703	956	1	30	1	45.8	65	50.264	168	56.32 %	DL2	13.9	183	atn	
20140703	958	1	30	2	45.9	65	50.336	168	56.413 %	DL2	14.3	177	atn	T/S suspiciously constant...,
20140703	1009	1	31	1	46.5	65	51.256	168	56.227 %	DL3	10.7	222	atn	
20140703	1011	1	31	2	46.5	65	51.338	168	56.272 %	DL3	11.3	191	atn	
20140703	1028	1	32	1	44.3	65	52.226	168	56.258 %	DL4	13.7	191	atn	
20140703	1030	1	32	2	44	65	52.268	168	56.329 %	DL4	14.2	173	atn	
20140703	1041	1	33	1	46.5	65	53.172	168	56.218 %	DL5	10.6	198	atn	
20140703	1044	1	33	2	46.7	65	53.243	168	56.291 %	DL5	13.3	189	atn	
20140703	1055	1	34	1	47.2	65	54.152	168	56.173 %	DL6	9.5	189	atn	
20140703	1058	1	34	2	47.1	65	54.253	168	56.148 %	DL6	14.4	196	atn	
20140703	1108	1	35	1	47.6	65	55.133	168	56.177 %	DL7	9.5	194	atn	
20140703	1110	1	35	2	47.4	65	55.208	168	56.239 %	DL7	8.9	189	atn	
20140703	1121	1	36	1	48.1	65	56.114	168	56.185 %	DL8	10.5	214	atn	nice reversal of T (colder at surface)
20140703	1123	1	36	2	48.2	65	56.202	168	56.224 %	DL8	9.4	198	atn	upcast quite different near surface
20140703	1133	1	37	1	49.1	65	57.097	168	56.201 %	DL9	12.5	202	atn	
20140703	1136	1	37	2	49.1	65	57.185	168	56.227 %	DL9	11.8	192	atn	
20140703	1145	1	38	1	50.1	65	58.064	168	56.202 %	DL10	14.3	207	atn	
20140703	1148	1	38	2	50.1	65	58.151	168	56.223 %	DL10	16.4	202	atn	upcast catching warmer water..
20140703	1157	1	39	1	50.5	65	59.048	168	56.179 %	DL11	14.3	208	atn	
20140703	1200	1	39	2	50.4	65	59.162	168	56.198 %	DL11	13.5	201	atn	
20140703	1210	1	40	1	50.9	66	0.03	168	56.2 %	DL12	14.7	209	ACPF	
20140703	1212	1	40	2	50.9	66	0.08	168	56.2 %	DL12	14.4	196	ACPF	
% Wrong xmlcon file (BStrait14031, instead of *_v3.xmlcon) on casts prior to this. Corrected here.														
20140703	1232	1	41	1	51.2	66	2.56	168	56.24 %	DL13	15.5	205	ACPF	Stations more spaced now.

20140703	1235	1	41	2	51.2	66	2.66	168	56.3 %	DL13	15.3	196	ACPF	
20140703	1255	1	42	1	53.1	66	5.11	168	56.2 %	DL14	16.2	204	ACPF	T-S ~ constant with depth, but T1=T2, S1=S2. Is ok.
20140703	1257	1	42	2	53.2	66	5.19	168	56.22 %	DL14	16	194	ACPF	
20140703	1316	1	43	1	53.1	66	7.66	168	56.2 %	DL15	18.1	201	ACPF	Water column well T-S mixed.
20140703	1319	1	43	2	53	66	7.75	168	56.24 %	DL15	17.8	191	ACPF	
20140703	1337	1	44	1	52.9	66	10.2	168	56.11 %	DL16	13.6	202	ACPF	Finally some T-S structure here, with halocline.
20140703	1340	1	44	2	53.1	66	10.31	168	56.09 %	DL16	20.5	196	ACPF	
20140703	1358	1	45	1	55.3	66	12.73	168	56.23 %	DL17	22.2	207	ACPF	Winds and swell picking up...
20140703	1400	1	45	2	54.7	66	12.8	168	56.27 %	DL17	20.7	190	ACPF	
20140703	1420	1	46	1	55.7	66	15.37	168	56.09 %	DL18	20.5	208	ACPF	Big swell, stopped well above bottom (at 51 m)
20140703	1423	1	46	2	55.6	66	15.43	168	56.06 %	DL18	18.9	210	ACPF	
20140703	1441	1	47	1	54.6	66	17.98	168	56.09 %	DL19	19	201	ACPF	Swell calmed. Likely touched bottom, but package ok on recovery.
20140703	1444	1	47	2	54.7	66	18.05	168	56.09 %	DL19	18.5	203	ACPF	END OF DL line
20140703	1458	1	48	1	54.6	66	19.73	168	56.99 %	A3-14	20.9	193	ACPF	START OF AL line NE bound
20140703	1500	1	48	2	54.4	66	19.79	168	56.96 %	A3-14	22.1	190	ACPF	** Hdr files have wrong station IDs on this line (1 station off).
20140703	1513	1	49	1	54.1	66	20.496	168	53.647 %	AL13	22.8	188	RJD	
20140703	1517	1	49	2	54.3	66	20.615	168	53.701 %	AL13	22.7	190	RJD	
20140703	1533	1	50	1	53.6	66	21.16	168	49.46 %	AL14	18.2	197	ACPF	
20140703	1535	1	50	2	53.3	66	21.217	168	49.44 %	AL14	23.6	199	ACPF	
20140703	1550	1	51	1	45.7	66	21.84	168	45.21 %	AL15	20.7	194	ACPF	
20140703	1553	1	51	2	46	66	21.91	168	45.17 %	AL15	23.1	190	ACPF	
20140703	1609	1	52	1	56.2	66	22.53	168	40.95 %	AL16	16.3	201	ACPF	Winds and seas calming down quite fast
20140703	1612	1	52	2	56	66	22.58	168	40.93 %	AL16	18.8	208	ACPF	
20140703	1628	1	53	1	54	66	23.26	168	36.55 %	AL17	16.5	185	ACPF	very smooth profile
20140703	1631	1	53	2	54	66	23.31	168	36.62 %	AL17	17	193	ACPF	
20140703	1649	1	54	1	51.6	66	23.97	168	32.28 %	AL18	15.6	188	ACPF	
20140703	1652	1	54	2	51.9	66	23.98	168	32.35 %	AL18	16.4	193	ACPF	
20140703	1709	1	55	1	52.6	66	24.69	168	27.9 %	AL19	14.9	183	ACPF	Homogeneous T&S all through depth
20140703	1712	1	55	2	52.6	66	24.71	168	27.94 %	AL19	14.9	183	ACPF	
20140703	1727	1	56	1	51.2	66	25.36	168	23.62 %	AL20	16.7	185	ACPF	Nearly-homogeneous T&S all through depth
20140703	1730	1	56	2	51.2	66	25.39	168	23.65 %	AL20	16.2	180	ACPF	
20140703	1743	1	57	1	46.5	66	26	168	19.37 %	AL21	16.2	194	ACPF	
20140703	1746	1	57	2	46.3	66	26.01	168	19.31 %	AL21	17	200	ACPF	
20140703	1800	1	58	1	39.6	66	26.71	168	14.95 %	AL22	16.4	194	ACPF	
20140703	1802	1	58	2	39.4	66	26.73	168	14.9 %	AL22	19.4	198	ACPF	
20140703	1815	1	59	1	32.3	66	27.42	168	10.72 %	AL23	18.5	200	ACPF	
20140703	1817	1	59	2	32.3	66	27.42	168	10.67 %	AL23	18.5	200	ACPF	
20140703	1834	1	60	1	26	66	28.23	168	6.14 %	AL24	19.4	190	ACPF	Hdr file has AL24ok. Calmer, Perhaps touched bottom.
20140703	1836	1	60	2	26	66	28.24	168	6.18 %	AL24	19.1	191	ACPF	END OF AL line...
20140704	204	1	61	1	48.7	67	38.009	168	55.984 %	CS10US	16.5	174	RJD	START OF CS line NE bound
20140704	207	1	61	2	48.7	67	38.117	168	55.738 %	CS10US	16.6	172	RJD	
20140704	236	1	62	1	48.5	67	40.678	168	48.114 %	CS10.5	16.2	171	RJD	
20140704	238	1	62	2	48.3	67	40.733	168	48.094 %	CS10.5	17.6	183	RJD	
20140704	319	1	63	1	48.5	67	45.263	168	39.943 %	CS11	14.1	191	RJD	
20140704	322	1	63	2	48.5	67	45.298	168	39.913 %	CS11	13.7	180	RJD	
20140704	404	1	64	1	49.4	67	48.886	168	29.529 %	CS11.5	12.4	145	RJD	
20140704	406	1	64	2	49.3	67	48.929	168	29.52 %	CS11.5	9.7	148	RJD	
20140704	446	1	65	1	54.6	67	52.467	168	18.977 %	CS12	17.2	164	atn	
20140704	448	1	65	2	54.7	67	52.489	168	18.936 %	CS12	16.5	179	atn	
20140704	525	1	66	1	57.5	67	55.847	168	9.285 %	CS12.5	18.9	173	atn	
20140704	528	1	66	2	57.2	67	55.882	168	9.277 %	CS12.5	17.1	174	atn	
20140704	606	1	67	1	52.9	67	59.267	167	59.58 %	CS13	15.8	146	atn	
20140704	609	1	67	2	53.2	67	59.311	167	59.642 %	CS13	14.5	152	atn	
20140704	648	1	68	1	52.2	68	2.667	167	49.877 %	CS13.5	19.4	159	atn	
20140704	651	1	68	2	52.3	68	2.706	167	49.882 %	CS13.5	18	165	atn	ship moved on upcast for wire angle. Note zigzag on upcast.
20140704	728	1	69	1	50.9	68	6.06	167	40.057 %	CS14	19.4	161	atn	7degC water!
20140704	730	1	69	2	50.6	68	6.104	167	40.1 %	CS14	17.9	165	atn	
20140704	807	1	70	1	47	68	9.078	167	30.856 %	CS14.5	19.3	178	atn	

20140704	809	1	70	2	47.2	68	9.122	167	30.815 %	CS14.5	18.8	185	atn	
20140704	852	1	71	1	46.1	68	12.06	167	21.527 %	CS15	16.8	181	atn	
20140704	854	1	71	2	46.1	68	12.081	167	21.492 %	CS15	17.8	190	atn	
20140704	912	1	72	1	44.3	68	13.553	167	16.894 %	CS15.5	16.7	183	atn	
20140704	915	1	72	2	44.7	68	13.572	167	16.832 %	CS15.5	16.8	191	atn	
20140704	933	1	73	1	43.2	68	14.958	167	12.262 %	CS16	15.4	182	atn	
20140704	935	1	73	2	43.3	68	14.976	167	12.204 %	CS16	15.7	189	atn	
20140704	954	1	74	1	40.1	68	16.555	167	7.669 %	CS16.5	14.2	171	atn	
20140704	956	1	74	2	40.1	68	16.568	167	7.602 %	CS16.5	14.3	193	atn	
20140704	1013	1	75	1	37.1	68	17.964	167	2.991 %	CS17	16.5	190	atn	
20140704	1015	1	75	2	36.5	68	17.976	167	2.929 %	CS17	17.4	186	atn	
20140704	1034	1	76	1	32.4	68	18.893	166	57.748 %	CS18	14.1	193	atn	
20140704	1036	1	76	2	32.1	68	18.912	166	57.773 %	CS18	14.1	192	atn	
20140704	1100	1	77	1	25.1	68	19.867	166	52.465 %	CS19	14.9	180	atn	
20140704	1103	1	77	2	25.3	68	19.886	166	52.525 %	CS19	12.9	182	atn	END OF CS line
20140704	1615	1	78	1	26.3	68	54.45	166	19.85 %	LIS1	15.9	192	ACPF	START OF LIS line W-bound
20140704	1617	1	78	2	26.5	68	54.48	166	19.84 %	LIS1	15.6	187	ACPF	deeper (~25m) thermoclines
20140704	1631	1	79	1	31	68	54.82	166	25.13 %	LIS2	15.4	197	ACPF	deeper (~25m) thermoclines
20140704	1634	1	79	2	30.9	68	54.82	166	25.16 %	LIS2	15.5	196	ACPF	
20140704	1648	1	80	1	32.2	68	55.26	166	30.48 %	LIS3	13.3	190	ACPF	
20140704	1650	1	80	2	32.4	68	55.21	166	30.59 %	LIS3	15.6	195	ACPF	
20140704	1710	1	81	1	40.1	68	55.82	166	38.5 %	LIS4	15.8	187	ACPF	Half a s blanking of screen during upcast near surface. Out of water?
20140704	1712	1	81	2	40.1	68	55.84	166	38.53 %	LIS4	15.4	185	ACPF	
20140704	1733	1	82	1	44.3	68	56.44	166	46.54 %	LIS5	16.7	179	ACPF	
20140704	1736	1	82	2	44.2	68	56.47	166	46.56 %	LIS5	17.9	183	ACPF	
20140704	1758	1	83	1	45.2	68	56.98	166	54.56 %	LIS6	16.5	199	ACPF	
20140704	1800	1	83	2	45.2	68	57	166	54.5 %	LIS6	16.6	186	ACPF	
20140704	1820	1	84	1	45.2	68	57.61	167	1.2 %	LIS6.5	15.6	188	ACPF	Hdr mislabelled as LIS7, but correct is LIS6.5
20140704	1823	1	84	2	44.9	68	57.62	167	1.22 %	LIS6.5	16.8	184	ACPF	
20140704	1844	1	85	1	45.1	68	58.23	167	9.29 %	LIS7	17	180	ACPF	
20140704	1846	1	85	2	45.1	68	58.24	167	9.3 %	LIS7	16.7	193	ACPF	
20140704	1906	1	86	1	45.3	68	58.82	167	16.57 %	LIS7.5	15.5	184	ACPF	
20140704	1908	1	86	2	45.3	68	58.83	167	16.62 %	LIS7.5	18	178	ACPF	
20140704	1927	1	87	1	45.8	68	59.41	167	23.95 %	LIS8	14.3	188	ACPF	
20140704	1930	1	87	2	45.9	68	59.41	167	23.97 %	LIS8	16.6	187	ACPF	
20140704	2015	1	88	1	47.1	69	0.643	167	38.767 %	LIS9	16.5	175	RJD	
20140704	2018	1	88	2	47.3	69	0.678	167	38.707 %	LIS9	17.3	192	RJD	
20140704	2056	1	89	1	47.7	69	1.808	167	53.356 %	LIS10	13.4	187	RJD	
20140704	2058	1	89	2	47.8	69	1.83	167	53.264 %	LIS10	15.9	173	RJD	
20140704	2136	1	90	1	48.5	69	1.36	168	7.927 %	LIS11	13.9	183	RJD	Hex file lost (2 copies of seasave open?)
20140704	2138	1	90	2	48.7	69	1.388	168	7.9 %	LIS11	14.1	180	RJD	
20140704	2205	1	91	1	48.6	69	1.386	168	8.062 %	LIS11	15.7	183	RJD	recast of LIS11
20140704	2208	1	91	2	48.6	69	1.427	168	8.012 %	LIS11	14.5	185	RJD	
20140704	2245	1	92	1	49	69	0.901	168	22.4 %	LIS12	15.8	167	RJD	
20140704	2247	1	92	2	49	69	0.93	168	22.436 %	LIS12	12.6	177	RJD	
20140704	2323	1	93	1	50.2	69	0.443	168	36.989 %	LIS13	14.3	177	RJD	
20140704	2325	1	93	2	50.7	69	0.46	168	36.927 %	LIS13	11.5	167	RJD	
20140704	2353	1	94	1	50.9	69	0.241	168	46.666 %	LIS14	15.8	168	RJD	
20140704	2355	1	94	2	50.8	69	0.274	168	46.707 %	LIS14	14.3	167	RJD	END OF LIS line
20140705	19	1	95	1	51	69	59.982	168	55.922 %	CCL22	12.7	173	RJD	START OF CCL line S bound
20140705	21	1	95	2	51.1	69	0.002	168	55.931 %	CCL22	11.4	171	RJD	
20140705	144	1	96	1	51.6	68	50.031	168	55.976 %	CCL21	13.8	190	RJD	
20140705	147	1	96	2	51.6	68	50.067	168	55.905 %	CCL21	13.9	188	RJD	
20140705	327	1	97	1	51.3	68	40.074	168	55.999 %	CCL20	13	184	RJD	
20140705	331	1	97	2	51.3	68	40.05	168	56.089 %	CCL20	13.1	194	RJD	
20140705	452	1	98	1	53.4	68	30.057	168	56.012 %	CCL19	10.8	189	atn	
20140705	454	1	98	2	53.2	68	30.033	168	56.127 %	CCL19	11.5	191	atn	
20140705	615	1	99	1	54.4	68	20.07	168	56.038 %	CCL18	10.9	181	atn	

20140705	618	1	99	2	54.5	68	20.04	168	56.152 %	CCL18	9.3	190 atn	Sucked up something at depth? (S spike upcast)
20140705	736	1	100	1	56	68	10.054	168	56.044 %	CCL17	6.8	184 atn	
20140705	739	1	100	2	56.1	68	10.008	168	56.177 %	CCL17	7.3	182 atn	
20140705	858	1	101	1	55.8	68	0.055	168	56.025 %	CCL16	6.9	141 atn	
20140705	901	1	101	2	55.7	67	59.98	168	56.102 %	CCL16	6.4	155 atn	
20140705	1016	1	102	1	49.2	67	50.067	168	56.014 %	CCL15	5.5	134 atn	
20140705	1019	1	102	2	49.3	67	50.005	168	56.05 %	CCL15	5.2	137 atn	
20140705	1146	1	103	1	48.7	67	38.232	168	56.084 %	CCL14	4.5	133 atn	
20140705	1148	1	103	2	48.7	67	38.251	168	56.227 %	CCL14	2.9	141 atn	
20140705	1249	1	104	1	48.3	67	30.4	168	55.99 %	CCL13	4.1	154 ACPF	
20140705	1251	1	104	2	48.3	67	30.01	168	56.02 %	CCL13	3.9	165 ACPF	
20140705	1405	1	105	1	47.9	67	20.07	168	55.99 %	CCL12	1.5	317 ACPF	
20140705	1407	1	105	2	47.9	67	19.98	168	55.91 %	CCL12	1.7	322 ACPF	
20140705	1516	1	106	1	47.1	67	10.06	168	55.99 %	CCL11	2.6	112 ACPF	
20140705	1518	1	106	2	47.1	67	10.07	168	55.88 %	CCL11	2.8	7.1 ACPF	
20140705	1630	1	107	1	46.1	66	59.99	168	56.03 %	CCL10	1.5	82 ACPF	
20140705	1632	1	107	2	46.1	66	59.97	168	55.96 %	CCL10	2	74 ACPF	
20140705	1743	1	108	1	43.2	66	50.08	168	56 %	CCL9	1.7	301 ACPF	
20140705	1745	1	108	2	43.3	66	49.98	168	55.9 %	CCL9	1.3	289 ACPF	
20140705	1854	1	109	1	41.9	66	39.99	168	56.02 %	CCL8	6.4	289 ACPF	
20140705	1856	1	109	2	41.8	66	39.94	168	56.22 %	CCL8	7.4	296 ACPF	
20140705	1932	1	110	1	44.3	66	35.02	168	56.1 %	CCL7	7.1	317 ACPF	
20140705	1935	1	110	2	44.2	66	34.98	168	56.18 %	CCL7	6.7	315 ACPF	
20140705	2010	1	111	1	55	66	30.003	168	56.058 %	CCL6	4.4	349 RJD	
20140705	2013	1	111	2	55.1	66	29.964	168	56.186 %	CCL6	4.8	356 RJD	
20140705	2047	1	112	1	54.6	66	24.977	168	56.152 %	CCL5	4.8	346 RJD	
20140705	2050	1	112	2	54.9	66	24.943	168	56.358 %	CCL5	5.2	350 RJD	
20140705	2109	1	113	1	53.9	66	22.301	168	56.112 %	CCL4	4.5	6 RJD	
20140705	2112	1	113	2	53.8	66	22.323	168	56.23 %	CCL4	5.1	13 RJD	
20140705	2131	1	114	1	54.4	66	19.686	168	56.894 %	A3	3.5	16 RJD	
20140705	2134	1	114	2	54.4	66	19.706	168	56.97 %	A3	3.7	11 RJD	END OF CCL line
20140705	2151	1	115	1	54.9	66	17.847	168	56.162 %	DL19	1.8	12 RJD	Start of DL line S bound
20140705	2153	1	115	2	54.8	66	17.899	168	56.115 %	DL19	1.5	348 RJD	
20140705	2215	1	116	1	55.8	66	15.284	168	56.316 %	DL18	1.2	306 RJD	
20140705	2217	1	116	2	55.8	66	15.308	168	56.529 %	DL18	0.9	335 RJD	
20140705	2237	1	117	1	55.4	66	12.724	168	56.272 %	DL17	3.2	344 RJD	
20140705	2240	1	117	2	55.4	66	12.664	168	56.331 %	DL17	3.7	346 RJD	
20140705	2300	1	118	1	54.3	66	10.183	168	56.15 %	DL16	6.1	334 RJD	
20140705	2302	1	118	2	54.3	66	10.222	168	56.166 %	DL16	6.1	327 RJD	
20140705	2324	1	119	1	52.9	66	7.615	168	56.294 %	DL15	1.4	4 RJD	
20140705	2326	1	119	2	52.9	66	7.55	168	56.283 %	DL15	4	345 RJD	
20140705	2344	1	120	1	53.9	66	5.145	168	56.23 %	DL14	2.1	27 RJD	
20140705	2348	1	120	2	53.3	66	5.126	168	56.42 %	DL14	2.275	31 RJD	
20140706	7	1	121	1	51.5	66	2.548	168	56.14 %	DL13	5.9	343 RJD	
20140706	9	1	121	2	51.3	66	2.597	168	56.001 %	DL13	5.6	342 RJD	
20140706	31	1	122	1	50.9	66	0.015	168	56.287 %	DL12	5.5	318 RJD	
20140706	34	1	122	2	50.8	65	59.999	168	56.361 %	DL12	5.6	318 RJD	
20140706	43	1	123	1	50.8	65	58.009	168	56.283 %	DL11	6.3	320 RJD	
20140706	46	1	123	2	50.4	65	58.979	168	56.339 %	DL11	6.1	322 RJD	
20140706	54	1	124	1	50.3	65	58.083	168	56.166 %	DL10	6	317 RJD	
20140706	57	1	124	2	50.4	65	58.049	168	56.163 %	DL10	6.6	323 RJD	
20140706	106	1	125	1	49.4	65	57.124	168	56.136 %	DL9	4.2	328 RJD	
20140706	109	1	125	2	49.6	65	57.13	168	55.963 %	DL9	6.2	319 RJD	
20140706	119	1	126	1	48.3	65	56.092	168	56.289 %	DL8	6.7	330 RJD	
20140706	121	1	126	2	48.3	65	56.058	168	56.322 %	DL8	6.3	323 RJD	
20140706	130	1	127	1	47.6	65	55.132	168	56.327 %	DL7	5.8	330 RJD	
20140706	133	1	127	2	47.8	65	55.146	168	56.439 %	DL7	5.8	333 RJD	
20140706	142	1	128	1	47.6	65	54.15	168	56.327 %	DL6	6.7	332 RJD	

20140706	145	1	128	2	47.5	65	54.11	168	56.305 %	DL6	5.2	325	RJD	
20140706	153	1	129	1	46.8	65	53.195	168	56.25 %	DL5	6.2	325	RJD	
20140706	156	1	129	2	46.7	65	53.18	168	56.139 %	DL5	6.1	308	RJD	
20140706	205	1	130	1	44.5	65	52.252	168	56.27 %	DL4	6.6	323	RJD	
20140706	207	1	130	2	44.1	65	52.247	168	56.454 %	DL4	7.6	338	RJD	
20140706	216	1	131	1	46.7	65	51.241	168	56.293 %	DL3	4.7	333	RJD	
20140706	221	1	131	2	46.6	65	51.249	168	56.546 %	DL3	5.5	339	RJD	
20140706	230	1	132	1	46.3	65	50.336	168	56.298 %	DL2	4.5	303	RJD	
20140706	232	1	132	2	45.9	65	50.371	168	56.389 %	DL2	4.7	306	RJD	
20140706	243	1	133	1	45.7	65	49.368	168	56.29 %	DL1	6.3	313	RJD	
20140706	245	1	133	2	45.5	65	49.403	168	56.327 %	DL1	5.9	306	RJD	END OF DL line
20140706	301	1	134	1	43.4	65	49.273	168	52.309 %	DLa1	7.2	322	atn	Start of DLa Line
20140706	303	1	134	2	43.4	65	49.221	168	52.287 %	DLa1	7.7	325	atn	
20140706	313	1	135	1	45.3	65	50.255	168	52.089 %	DLa2	7.4	320	RJD	
20140706	315	1	135	2	46.3	65	50.317	168	51.884 %	DLa2	6.6	335	RJD	
20140706	323	1	136	1	47.5	65	51.226	168	52.19 %	DLa3	6.5	340	RJD	
20140706	325	1	136	2	47.5	65	51.296	168	52.256 %	DLa3	7	335	RJD	
20140706	333	1	137	1	48.1	65	52.194	168	52.144 %	DLa4	6.4	336	RJD	
20140706	335	1	137	2	48.1	65	52.22	168	51.999 %	DLa4	6.5	344	RJD	
20140706	344	1	138	1	48.2	65	53.136	168	52.103 %	DLa5	7.3	350	RJD	
20140706	346	1	138	2	46.8	65	53.13	168	51.975 %	DLa5	7.1	359	RJD	
20140706	356	1	139	1	48.3	65	54.12	168	52.216 %	DLa6	6.7	348	RJD	
20140706	358	1	139	2	48.1	65	54.154	168	52.081 %	DLa6	6.1	356	RJD	.hdr file mislabeled as DLa5, should be DLa6
20140706	408	1	140	1	49.3	65	55.161	168	52.29 %	DLa7	5.8	348	atn	
20140706	411	1	140	2	49.5	65	55.148	168	52.21 %	DLa7	3.2	3	atn	
20140706	420	1	141	1	50.4	65	56.089	168	52.205 %	DLa8	5.7	358	atn	
20140706	422	1	141	2	50.6	65	56.124	168	52.026 %	DLa8	5.7	6	atn	
20140706	431	1	142	1	50.3	65	57.114	168	52.227 %	DLa9	6.1	5	atn	
20140706	434	1	142	2	50.3	65	57.104	168	52.223 %	DLa9	6.1	14	atn	
20140706	442	1	143	1	50.6	65	58.011	168	52.233 %	DLa10	6.7	357	atn	
20140706	444	1	143	2	50.7	65	58.043	168	52.067 %	DLa10	5.9	8	atn	
20140706	455	1	144	1	50.8	65	59.047	168	52.226 %	DLa11	5.3	8	atn	
20140706	457	1	144	2	50.8	65	59.054	168	52.1 %	DLa11	5.7	14	atn	
20140706	511	1	145	1	51.3	65	59.966	168	52.199 %	DLa12	6.4	28	atn	
20140706	513	1	145	2	51.1	65	59.974	168	52.294 %	DLa12	4.6	12	atn	End of DLa Line
20140706	527	1	146	1	51.6	65	59.999	168	48.235 %	DLa12	6.1	356	atn	Start of DLb Line
20140706	530	1	146	2	51.6	66	0.042	168	48.203 %	DLb12	6.5	3	atn	
20140706	539	1	147	1	52.2	65	59.091	168	48.209 %	DLb11	7.5	348	atn	
20140706	542	1	147	2	51.9	65	59.019	168	48.311 %	DLb11	7.7	348	atn	
20140706	551	1	148	1	51.3	65	58.111	168	48.183 %	DLb10	9.5	345	atn	
20140706	553	1	148	2	51.4	65	58.118	168	48.287 %	DLb10	8.8	357	atn	
20140706	604	1	149	1	51.4	65	57.149	168	48.264 %	DLb9	9.2	352	atn	nice multi-layers, multiple mixed events?
20140706	606	1	149	2	51.4	65	57.159	168	48.399 %	DLb9	9.2	358	atn	
20140706	617	1	150	1	51.4	65	56.158	168	48.159 %	DLb8	8.2	351	atn	
20140706	619	1	150	2	51.4	65	56.166	168	48.295 %	DLb8	8.2	2	atn	
20140706	630	1	151	1	51.6	65	55.156	168	48.181 %	DLb7	7.1	3	atn	
20140706	632	1	151	2	51.7	65	55.124	168	48.353 %	DLb7	7.9	15	atn	
20140706	642	1	152	1	51	65	54.21	168	48.234 %	DLb6	9.7	3	atn	
20140706	644	1	152	2	51.1	65	54.244	168	48.394 %	DLb6	9.4	13	atn	
20140706	655	1	153	1	50.7	65	53.186	168	48.12 %	DLb5	9.5	18	atn	BIG signal of turbidity + fluoro at bottom
20140706	658	1	153	2	50.8	65	53.122	168	48.005 %	DLb5	9.3	11	atn	
20140706	706	1	154	1	50.2	65	52.249	168	48.244 %	DLb4	9.9	9	atn	interesting warm+saline layer at bottom
20140706	709	1	154	2	50	65	52.266	168	48.373 %	DLb4	9.2	17	atn	
20140706	719	1	155	1	49.1	65	51.285	168	48.191 %	DLb3	7	4	atn	
20140706	721	1	155	2	48.9	65	51.265	168	48.293 %	DLb3	8.6	4	atn	
20140706	733	1	156	1	48.9	65	50.303	168	48.203 %	DLb2	7.1	351	atn	
20140706	735	1	156	2	49.1	65	50.308	168	48.344 %	DLb2	8.8	0	atn	
20140706	746	1	157	1	48.7	65	49.335	168	48.234 %	DLb1	9.9	349	atn	

20140706	749	1	157	2	48.5	65	49.374	168	48.391 %	DLb1	8.6	6 atn	END OF DLb line
20140706	916	1	158	1	50.7	66	0.04	168	55.885 %	NBS1	9.4	17 atn	START OF NBS Line, E bound
20140706	918	1	158	2	50.5	66	0.083	168	55.914 %	NBS1	9.8	12 atn	
20140706	929	1	159	1	50.8	66	0.016	168	52.996 %	NBS1.5	10.1	357 atn	
20140706	932	1	159	2	50.8	66	0.056	168	52.834 %	NBS1.5	10.2	356 atn	
20140706	942	1	160	1	51.6	65	59.98	168	49.849 %	NBS2	9.8	356 atn	
20140706	945	1	160	2	51.7	66	0.01	168	49.692 %	NBS2	9.7	359 atn	
20140706	957	1	161	1	51.7	66	0.024	168	45.838 %	NBS2.5	9.8	0 atn	
20140706	1000	1	161	2	51.8	66	0.088	168	45.684 %	NBS2.5	10.3	3 atn	
20140706	1013	1	162	1	51.6	65	59.971	168	41.692 %	NBS3	9.1	356 atn	
20140706	1015	1	162	2	51.6	66	0.014	168	41.515 %	NBS3	9.7	350 atn	
20140706	1029	1	163	1	51.1	65	59.973	168	37.47 %	NBS3.5	9.3	5 atn	
20140706	1031	1	163	2	51.3	66	0.011	168	37.315 %	NBS3.5	9.3	359 atn	
20140706	1045	1	164	1	51.7	65	59.901	168	33.315 %	NBS4	10.9	357 atn	
20140706	1048	1	164	2	52	65	59.949	168	33.207 %	NBS4	9.5	352 atn	
20140706	1101	1	165	1	52	65	59.992	168	29.15 %	NBS4.5	11.6	354 atn	
20140706	1104	1	165	2	51.6	66	0.056	168	29.048 %	NBS4.5	10.2	351 atn	
20140706	1117	1	166	1	55.4	66	0	168	25.092 %	NBS5	11.8	352 atn	
20140706	1120	1	166	2	55.4	66	0.053	168	24.962 %	NBS5	11.3	348 atn	
20140706	1134	1	167	1	52.2	65	59.992	168	20.818 %	NBS5.5	10.6	353 atn	
20140706	1137	1	167	2	52.2	66	0.036	168	20.681 %	NBS5.5	10.6	350 atn	
20140706	1151	1	168	1	51.2	65	59.995	168	16.464 %	NBS6	10.5	0 atn	
20140706	1154	1	168	2	51.1	66	0.039	168	16.292 %	NBS6	11.5	357 atn	
20140706	1212	1	169	1	48.3	65	59.98	168	12.51 %	NBS6.5	10.5	356 ACPF	
20140706	1214	1	169	2	48.2	65	59.97	168	12.35 %	NBS6.5	11.9	344 ACPF	
20140706	1227	1	170	1	45.8	66	0	168	8.6 %	NBS7	8.1	6 ACPF	
20140706	1229	1	170	2	45.4	66	0.04	168	8.43 %	NBS7	10.1	0 ACPF	
20140706	1244	1	171	1	38.4	66	0	168	4.32 %	NBS7.5	10.5	1 ACPF	
20140706	1246	1	171	2	38.3	66	0.04	168	4.16 %	NBS7.5	10.7	359 ACPF	
20140706	1303	1	172	1	32	66	0.01	168	0.11 %	NBS8	12.2	17 ACPF	
20140706	1304	1	172	2	31.9	66	0	167	59.98 %	NBS8	11.9	30 ACPF	
20140706	1321	1	173	1	19.7	65	59.98	167	55.28 %	NBS9	12.8	13 ACPF	
20140706	1323	1	173	2	19.6	66	0.01	167	55.21 %	NBS9	12.1	13 ACPF	END OF NBS line
20140706	1623	1	174	1	46.8	65	52.08	168	55.88 %	MBSn1	14.8	350 ACPF	START OF MBSn line E bound
20140706	1625	1	174	2	46.8	65	52.07	168	55.86 %	MBSn1	13.6	355 ACPF	
20140706	1636	1	175	1	47.7	65	52.02	168	52.63 %	MBSn1.5	11.7	2 ACPF	
20140706	1638	1	175	2	47.7	65	52.07	168	52.58 %	MBSn1.5	13.9	12 ACPF	
20140706	1652	1	176	1	49.1	65	51.85	168	49.15 %	MBSn2	13.2	4 ACPF	
20140706	1654	1	176	2	49.1	65	51.86	168	49.11 %	MBSn2	13.7	0 ACPF	
20140706	1709	1	177	1	51	65	51.76	168	45.04 %	MBSn2.5	14.1	2 ACPF	
20140706	1711	1	177	2	51.2	65	51.8	168	45 %	MBSn2.5	14.9	4 ACPF	
20140706	1727	1	178	1	51.2	65	51.68	168	40.98 %	MBSn3	16	0 ACPF	
20140706	1730	1	178	2	51.2	65	51.7	168	40.96 %	MBSn3	17	353 ACPF	
20140706	1745	1	179	1	51.7	65	51.57	168	36.49 %	MBSn3.5	15.4	359 ACPF	
20140706	1747	1	179	2	51.7	65	51.6	168	36.43 %	MBSn3.5	15.8	356 ACPF	
20140706	1804	1	180	1	51.4	65	51.48	168	31.99 %	MBSn4	14.9	1 ACPF	
20140706	1806	1	180	2	51.4	65	51.51	168	31.92 %	MBSn4	12.9	355 ACPF	
20140706	1822	1	181	1	54	65	51.37	168	27.61 %	MBSn4.5	12.2	16 ACPF	
20140706	1825	1	181	2	54.3	65	51.41	168	27.55 %	MBSn4.5	14.1	17 ACPF	
20140706	1842	1	182	1	50.2	65	51.3	168	23.06 %	MBSn5	12.4	8 ACPF	
20140706	1844	1	182	2	50.2	65	51.34	168	23.01 %	MBSn5	13.6	0 ACPF	
20140706	1901	1	183	1	48.6	65	51.19	168	18.56 %	MBSn5.5	12.5	351 ACPF	
20140706	1903	1	183	2	48.3	65	51.22	168	18.49 %	MBSn5.5	14.6	354 ACPF	
20140706	1919	1	184	1	45	65	51.08	168	13.96 %	MBSn6	12.5	356 ACPF	
20140706	1921	1	184	2	44.8	65	51.12	168	13.9 %	MBSn6	16.9	354 ACPF	
20140706	1934	1	185	1	44	65	51.08	168	10.45 %	MBSn6.5	12.8	359 ACPF	
20140706	1936	1	185	2	44	65	51.11	168	10.4 %	MBSn6.5	12.3	2 ACPF	
20140706	1949	1	186	1	37.4	65	50.96	168	6.96 %	MBSn7	12.8	14 ACPF	

20140706	1951	1	186	2	37.5	65	50.98	168	6.93 %	MBSn7	14.5	18	ACPF	
20140706	2000	1	187	1	28.7	65	50.86	168	5.09 %	MBSn8	12	10	ACPF	
20140706	2002	1	187	2	28.9	65	50.88	168	5.06 %	MBSn8	13.5	20	ACPF	END OF MBSn line
20140706	2244	1	188	1	45.4	65	48.31	168	55.461 %	BS11	11.5	319	RJD	START OF BS line E bound
20140706	2247	1	188	2	45.1	65	48.304	168	55.35 %	BS11	10.9	320	RJD	
20140706	2255	1	189	1	46	65	47.814	168	53.817 %	BS11j	11.7	323	RJD	
20140706	2258	1	189	2	46.2	65	47.799	168	53.709 %	BS11j	12.2	326	RJD	
20140706	2307	1	190	1	42.7	65	47.267	168	51.67 %	BS12	12.2	321	RJD	
20140706	2309	1	190	2	42.9	65	47.295	168	51.606 %	BS12	13.3	318	RJD	
20140706	2318	1	191	1	47.5	65	46.854	168	49.714 %	BS12AJ	12.2	325	RJD	
20140706	2321	1	191	2	47.6	65	46.909	168	49.636 %	BS12AJ	12.4	320	RJD	
20140706	2331	1	192	1	50	65	46.365	168	47.656 %	BS13	14.4	329	RJD	
20140706	2333	1	192	2	50.1	65	46.389	168	47.6 %	BS13	15.7	328	RJD	
20140706	2344	1	193	1	49.1	65	45.858	168	45.547 %	BS13Z	13.5	338	RJD	
20140706	2346	1	193	2	50.2	65	45.872	168	45.565 %	BS13Z	15.3	351	RJD	
20140706	2357	1	194	1	51.3	65	45.295	168	43.245 %	BS14	17.1	332	RJD	
20140706	2359	1	194	2	51.1	65	45.304	168	43.182 %	BS14	17.2	330	RJD	
20140707	8	1	195	1	50.3	65	44.829	168	41.564 %	BS14J	18	336	RJD	
20140707	10	1	195	2	50.3	65	44.835	168	41.486 %	BS14J	18.4	337	RJD	
20140707	18	1	196	1	50.2	65	44.356	168	39.824 %	BS15	17.5	341	RJD	
20140707	21	1	196	2	50.1	65	44.364	168	39.753 %	BS15	15.1	336	RJD	
20140707	31	1	197	1	50.2	65	43.836	168	37.64 %	BS15J	14.9	337	RJD	
20140707	33	1	197	2	50.2	65	43.853	168	37.572 %	BS15J	16.9	336	RJD	
20140707	43	1	198	1	49.9	65	43.276	168	35.492 %	BS16	16.8	340	RJD	
20140707	46	1	198	2	49.9	65	43.276	168	35.456 %	BS16	16.9	340	RJD	
20140707	55	1	199	1	50.3	65	42.768	168	33.388 %	BS16J	17.2	330	RJD	
20140707	58	1	199	2	50.4	65	42.784	168	33.329 %	BS16J	16.3	340	RJD	
20140707	107	1	200	1	53.7	65	42.241	168	31.325 %	BS17	11.7	350	RJD	
20140707	110	1	200	2	53.5	65	42.276	168	31.2 %	BS17	13.8	342	RJD	
20140707	120	1	201	1	51.9	65	41.716	168	29.234 %	BS17S	14.2	352	RJD	
20140707	122	1	201	2	51.9	65	41.751	168	29.132 %	BS17S	15.3	347	RJD	
20140707	132	1	202	1	52.3	65	41.192	168	26.962 %	BS18	14.2	353	RJD	
20140707	135	1	202	2	52.5	65	41.213	168	26.922 %	BS18	13.8	350	RJD	
20140707	144	1	203	1	51	65	40.802	168	25.243 %	BS18J	12.6	348	RJD	
20140707	147	1	203	2	51.3	65	40.833	168	25.203 %	BS18J	13.6	350	RJD	
20140707	156	1	204	1	50.2	65	40.366	168	23.485 %	BS19	14.5	354	RJD	
20140707	158	1	204	2	50.2	65	40.396	168	23.448 %	BS19	14.6	356	RJD	
20140707	209	1	205	1	48.9	65	39.862	168	21.296 %	BS19H	11.3	359	RJD	
20140707	212	1	205	2	49.1	65	39.914	168	21.264 %	BS19H	13.1	350	RJD	
20140707	224	1	206	1	47.1	65	39.339	168	19.06 %	BS20	13.2	352	RJD	
20140707	226	1	206	2	47.1	65	39.382	168	19.036 %	BS20	13.7	352	RJD	
20140707	237	1	207	1	44.6	65	38.938	168	17.061 %	BS20J	13.4	353	RJD	
20140707	239	1	207	2	44.8	65	38.977	168	17.071 %	BS20J	13.6	348	RJD	
20140707	249	1	208	1	40.7	65	38.551	168	15.04 %	BS21	12.2	357	RJD	
20140707	251	1	208	2	40.7	65	38.587	168	15.05 %	BS21	13.7	350	RJD	
20140707	304	1	209	1	37.5	65	38.044	168	13.003 %	BS21A	13.4	6	atn	
20140707	306	1	209	2	37.6	65	38.077	168	13.025 %	BS21A	12.5	1	atn	
20140707	319	1	210	1	30.5	65	37.502	168	10.779 %	BS22	12.4	7	atn	
20140707	321	1	210	2	30.5	65	37.536	168	10.791 %	BS22	11.8	7	atn	
20140707	338	1	211	1	29.1	65	35.994	168	9.785 %	BS23	16.5	34	RJD	
20140707	340	1	211	2	29.3	65	36.023	168	9.85 %	BS23	14.6	30	RJD	
20140707	400	1	212	1	25	65	34.934	168	7.164 %	BS24	24.1	13	RJD	This is the same as SBS1
20140707	402	1	212	2	26.8	65	34.939	168	7.26 %	BS24	22.7	18	RJD	END of line BS
20140707	421	1	213	1	37	65	33.953	168	11.996 %	SBS2	19.5	22	atn	BEGIN of line SBS
20140707	423	1	213	2	37	65	33.96	168	11.974 %	SBS2	19.3	8	atn	
20140707	443	1	214	1	42.6	65	32.962	168	16.765 %	SBS3	18.2	9	atn	
20140707	445	1	214	2	42.8	65	32.968	168	16.767 %	SBS3	17.7	356	atn	
20140707	506	1	215	1	47	65	31.981	168	21.555 %	SBS4	19.1	4	atn	

20140707	508	1	215	2	47	65	31.985	168	21.531 %	SBS4	19.7	348 atn	
20140707	528	1	216	1	58.1	65	31.007	168	26.391 %	SBS5	18.9	11 atn	
20140707	531	1	216	2	58	65	31.011	168	26.391 %	SBS5	18.2	359 atn	
20140707	550	1	217	1	59.3	65	30.002	168	31.27 %	SBS6	17	8 atn	
20140707	553	1	217	2	59.3	65	29.986	168	31.22 %	SBS6	18.2	355 atn	
20140707	612	1	218	1	54.8	65	29.041	168	36.113 %	SBS7	18.5	4 atn	
20140707	615	1	218	2	54.9	65	29.037	168	36.112 %	SBS7	17.9	352 atn	
20140707	636	1	219	1	55.2	65	28.047	168	40.999 %	SBS8	18.8	352 atn	
20140707	638	1	219	2	55.1	65	28.025	168	41.106 %	SBS8	17.2	5 atn	STOP here
